# Self-heating of Supported Ru Catalysts as a Trigger for Hydrogen Production by Ammonia Oxidative Decomposition from Room Temperature

## Katsutoshi Nagaoka,<sup>a,\*</sup> Suguru Matsumoto,<sup>a</sup> Ryo Tasaki, Yuta Ogura,<sup>a</sup> Katsutoshi Sato<sup>a,b</sup>

<sup>a</sup> Division of Applied Chemistry, Department of Integrated Science and Technology, Faculty of Science and Technology, Oita University, 700 Dannoharu, Oita 870-1192, Japan <sup>b</sup>Elements Strategy Initiative for Catalysts and Batteries, Kyoto University, 1-30 Goryo-Ohara, Nishikyo-ku, Kyoto 615-8245, Japan.

\*Corresponding author: +81-(0)97-554-7979, nagaoka@oita-u.ac.jp

Abstract: We demonstrate hydrogen production by exposing  $NH_3$  and  $O_2$  at room temperature to acidic  $RuO_2/\gamma$ -Al<sub>2</sub>O<sub>3</sub> or reduced  $RuO_2/Ce_{0.5}Zr_{0.5}O_2$  catalyst. In these process, the catalysts are heated from room temperature to catalytic auto-ignition temperature of NH<sub>3</sub> oxidative decomposition and thus the reaction begin, because adsorption of NH<sub>3</sub> onto the catalyst and oxidation of Ru/Ce<sub>0.5</sub>Zr<sub>0.5</sub>O<sub>2-x</sub> are exothermic.

Keywords: hydrogen carrier, ammonia, hydrogen production.

## **1. Introduction**

Hydrogen produced from renewable energy has received a lot of attentions as a clean energy source and development of a hydrogen storage and transportation system using hydrogen carrier has been greatly demanded. Among different kinds of hydrogen carrier, NH<sub>3</sub> is regarded as one of the promising candidates, due to high hydrogen capacity, high energy density, low production cost, and ease of liquification at room temperature. Furthermore, a carbon-free hydrogen storage and transportation system could be realized by using NH<sub>3</sub> as hydrogen carrier. In this system, hydrogen produced from NH<sub>3</sub> is used in engines, turbines and fuel cells. However, use of NH<sub>3</sub> as a hydrogen carrier, peculiarly for transportable devices and household, has been limited owing to lack of an efficient process for producing hydrogen from NH<sub>3</sub>.

To solve this problem, it is necessary to develop a process that can be initiated rapidly, produces hydrogen from NH<sub>3</sub> at a high rate, and does not need external heat supply. NH<sub>3</sub> oxidative decomposition (Eq. 1) is a combination of NH<sub>3</sub> combustion (Eq. 2) and NH<sub>3</sub> decomposition (Eq. 3) and thus the heat generated by NH<sub>3</sub> combustion is utilized for NH<sub>3</sub> decomposition, which results in high hydrogen formation rate. Furthermore, after ignition of NH<sub>3</sub> oxidative decomposition at catalytic auto-ignition temperature, the catalyst is automatically heated to reaction temperature due to exothermic nature of the reaction and then the reaction proceeds spontaneously. Therefore, challenge is how to heat the catalyst from room temperature to catalytic auto-ignition temperature of NH<sub>3</sub> oxidative decomposition. In this research, we have discovered that the heat generated by self-heating of the catalyst heats the catalyst rapidly. Our results demonstrated that two kinds of heats are available for self-heating, i.e. heat produced by NH<sub>3</sub> adsorption on the catalyst<sup>1</sup> and oxidation of the reduced catalyst. With this process, hydrogen is produced by only supplying NH<sub>3</sub> and oxygen at room temperature to pre-treated oxide-supported Ru catalysts.

NH<sub>3</sub> (g) + 0.25O<sub>2</sub> (g)  $\rightarrow$  H<sub>2</sub> (g) + 0.5N<sub>2</sub> (g) + 0.5H<sub>2</sub>O (g)  $\Delta$ H = -75 kJ mol<sup>-1</sup> (Eq. 1)

NH<sub>3</sub> (g) + 0.75O<sub>2</sub> (g)  $\rightarrow$  0.5N<sub>2</sub> (g) + 1.5H<sub>2</sub>O (g)  $\Delta$ H = -317 kJ mol<sup>-1</sup> (Eq. 2)

 $NH_3(g) + 0.25O_2(g) \rightarrow H_2(g) + 0.5N_2(g) + 0.5H_2O(g) \Delta H = -75 \text{ kJ mol}^{-1}$  (Eq. 3)

We also succeeded in construction of cyclic process where NH<sub>3</sub> oxidative decomposition is triggered repeatedly without pre-treatment from 2<sup>nd</sup> cyvle.

#### 2. Experimental

 $RuO_2/\gamma$ -Al<sub>2</sub>O<sub>3</sub> and  $RuO_2/Ce_{0.5}Zr_{0.5}O_2$  were prepared by wet impregnation method.

After the pre-treatment shown in SS3, triggering tests were carried out under quasi-adiabatic conditions. An NH<sub>3</sub>/O<sub>2</sub>/He (NH<sub>3</sub>/O<sub>2</sub>/He ratio, 150:37.5:20.8 ml min<sup>-1</sup>;GHSV, 62.5 Lh<sup>-1</sup>g<sup>-1</sup>) gas mixture was then fed at room temperature to the catalyst. We set the gas composition assuming the Eq. 1. The composition of the exit gas was monitored with a quadrupole mass spectrometer. After 30 min, the composition of the dried exit gas was analyzed with a thermal conductivity detector.

### 3. Results and discussion

The RuO<sub>2</sub>/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> catalyst was treated in He at 300°C to remove adsorbate and create NH<sub>3</sub> adsorption site and then the catalyst was cooled to room temperature. After supplying the NH<sub>3</sub>/O<sub>2</sub>/He mixture, H<sub>2</sub> production rate increased to 33 Lh<sup>-1</sup>g<sup>-1</sup> within 30 s and catalyst bed temperature rose to 522 °C at the same time<sup>1</sup>. After the reaction for 30 min, O<sub>2</sub> was consumed completely: NH<sub>3</sub> conversion was 93% and hydrogen yield was near the maximum value, 67 % (Fig. 1A). These results demonstrate that NH<sub>3</sub> oxidative decomposition is triggered in a very short time without any external heat input and proceeds spontaneously. After 35 min, the reaction was terminated by substitution of He for the NH<sub>3</sub>/O<sub>2</sub>/He mixture, and the catalyst was cooled to room temperature. O<sub>2</sub> was then briefly supplied over the catalyst to oxidize the Ru metal formed during the reaction, and an NH<sub>3</sub>/O<sub>2</sub>/He mixture was fed to the catalyst. This purge-feed sequence was repeated three more times. For all cycles, the oxidative decomposition of ammonia was repeatedly triggered at room temperature, and high H<sub>2</sub> yields as well as high NH<sub>3</sub> and O<sub>2</sub> conversions were maintained. After the second cycle, ammonia was apparently desorbed *in situ* (regeneration of NH<sub>3</sub> adsorption sites) during the reaction.

On the other hand, RuO<sub>2</sub>/Ce<sub>0.5</sub>Zr<sub>0.5</sub>O<sub>2</sub> catalyst was treated in H<sub>2</sub> at room temperature to reduce the catalyst. After supplying the NH<sub>3</sub>/O<sub>2</sub>/He mixture, catalyst bed temperature increased drastically and H<sub>2</sub> production starts. After the reaction for 30 min, O<sub>2</sub> as well as NH<sub>3</sub> were consumed completely and H<sub>2</sub> yield reached 67 % (Fig. 1B). These results elucidate that NH<sub>3</sub> oxidative decomposition is triggered without any external heat input. After 35 min, the reaction was terminated by stopping the flow of O<sub>2</sub> and He in NH<sub>3</sub>/O<sub>2</sub>/He mixture, and the catalyst was cooled to room temperature. Then, an NH<sub>3</sub>/O<sub>2</sub>/He mixture was fed to the catalyst. This purge-feed sequence was repeated three more times. For all cycles, the oxidative decomposition of ammonia was repeatedly triggered at room temperature. After the second cycle, the catalyst was reduced to Ru/Ce<sub>0.5</sub>Zr<sub>0.5</sub>O<sub>2-x</sub> *in situ* during the reaction.



Figure 1. Cycle tests of NH<sub>3</sub> oxidative decomposition from room temperature over (A) RuO<sub>2</sub>/γ-Al<sub>2</sub>O<sub>3</sub> and (B) RuO<sub>2</sub>/Ce<sub>0.5</sub>Zr<sub>0.5</sub>O<sub>2</sub>.

### 4. Conclusions

Our results indicate that self-heating of the catalyst at room temperature is used as a trigger for the NH<sub>3</sub> oxidative decomposition. To heat the catalyst to the catalytic auto-ignition temperature, we successfully used the heat evolved by ammonia adsorption onto  $RuO_2/\gamma$ -Al<sub>2</sub>O<sub>3</sub> or oxidation of  $Ru/Ce_{0.5}Zr_{0.5}O_{2-x}$ . This study demonstrates the concept of self-heating of catalysts, which is a novel strategy for the cold-start process for hydrogen production from ammonia and other reactions.

#### Reference

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